

PREDICTING CALCIUM OXALATE SCALE

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ABSTRACT

Calcium oxalate scale is frequently encountered in the sugar refining and paper making processes. This paper outlines a simple index for the prediction of calcium oxalate scale. The development of a more refined index, based upon free ion concentrations, is also discussed.

INTRODUCTION

Most indices for predicting scale are derived from the definition of the solubility product for the scale in question. For example, the commonly used Calcite Saturation Level⁽¹⁾ and classic Langelier Saturation Index⁽²⁾ for predicting calcium carbonate scale are derived from the relationship:

$$\{Ca\} \{CO_3\} = K_{sp} \quad (1)$$

where $\{Ca\}$ is the calcium activity;

$\{CO_3\}$ is the carbonate activity; and

K_{sp} is the solubility product at the temperature evaluated.

The Saturation Level or Ratio is the ratio of the current ion activity product (IAP) to the ion activity product expected at equilibrium:

$$\text{Saturation Level} = \frac{\{Ca\} \{CO_3\}}{K_{sp}} = \frac{\text{IAP}}{\text{Solubility Product}} \quad (2)$$

It can be shown that the Langelier Saturation Index is the base ten logarithm of the Saturation Level, when the saturation level is calculated from the total analytical value for calcium, and carbonate is estimated from the total analytical value for alkalinity.

Saturation Levels indicate the driving force for scale formation with respect to equilibrium. If a water has a Saturation Level greater than 1.0, it is supersaturated with respect to the scale. If the Saturation Level is 1.0, the water is at equilibrium and would not be expected to form or dissolve scale. Waters with a Saturation Level less than 1.0 are undersaturated and might be expected to dissolve an existing scale.

Logarithmic indices have a similar interpretation. A water with a log index greater than 0.0 would be supersaturated with respect to the scale evaluated, and would have an increasing tendency to form the scale with increases in the index. A water with a log index of 0.0 would be at equilibrium. Scale would not be expected to form or dissolve. A negative index value would indicate that the water might tend to dissolve an existing scale.

Saturation Levels calculated by commercial computer programs are typically based upon the free ion concentrations (e.g. free calcium and free carbonate). The free ion concentrations are based upon the most likely distribution of species and subtract 'bound' ion concentrations from the total analytical values to obtain the free ion concentration.⁽¹⁾

This paper describes the derivation and development of indices for predicting calcium oxalate scale based upon analytical values, and based upon free ion concentrations using an ion association model. The indices derived in this paper are based upon the solubility product for calcium oxalate:

$$\{Ca\} \{C_2O_4\} = K_{sp} \quad (3)$$

where $\{Ca\}$ is the calcium activity;

$\{C_2O_4\}$ is the oxalate activity; and

K_{sp} is the solubility product for calcium oxalate at the temperature evaluated.

The simple Saturation Level is calculated from the expanded form of equation 3:

$$\text{Saturation Level} = \frac{\alpha_{Ca}(Ca) \alpha_{C_2O_4} (C_2O_4)}{K_{sp}} \quad (4)$$

K_{sp}

where α_{Ca} is the activity coefficient for the calcium ion;

$\alpha_{C_2O_4}$ is the activity coefficient for the oxalate ion;

(Ca) is the molal calcium concentration;

(C_2O_4) is the molal oxalate concentration; and

K_{sp} is the solubility product for calcium oxalate at the temperature evaluated.

The analytical value for calcium is used calcium concentration. The oxalate ion concentration must be estimated from the analytical value for total oxalic acid. This is done using an alpha distribution.⁽³⁾ The alpha distribution method calculates the ion fractions for a diprotic acid such as oxalic as follows:

$$[\text{Oxalic}_{\text{total}}] = [\text{H}_2\text{C}_2\text{O}_4] + [\text{HC}_2\text{O}_4^-] + [\text{C}_2\text{O}_4^{2-}] \quad (5)$$

$$\alpha_0 = [\text{H}_2\text{C}_2\text{O}_4]/[\text{Oxalic}_{\text{total}}] \quad (6)$$

$$\alpha_1 = [\text{HC}_2\text{O}_4^-]/[\text{Oxalic}_{\text{total}}] \quad (7)$$

$$\alpha_2 = [\text{C}_2\text{O}_4^{2-}]/[\text{Oxalic}_{\text{total}}] \quad (8)$$

$$\alpha_0 = \frac{[\text{H}]^2}{[\text{H}]^2 + K_1[\text{H}] + K_1 K_2} \quad (9)$$

$$\alpha_1 = \frac{K_1 [\text{H}]}{[\text{H}]^2 + K_1[\text{H}] + K_1 K_2} \quad (10)$$

$$\alpha_2 = \frac{K_1 K_2}{[\text{H}]^2 + K_1[\text{H}] + K_1 K_2} \quad (11)$$

$$[\text{C}_2\text{O}_4^{2-}] = \alpha_2 [\text{Oxalic}_{\text{total}}] \quad (12)$$

Figure 3 depicts a full distribution of oxalic acid species at 25 °C, as calculated using the alpha distribution method. Table 2 summarizes the α_2 versus temperature. Note that α_2 approaches a value of 1.0 in alkaline waters, and can be assumed to be 1.0 above a pH of 8.

Activity coefficients for calcium and oxalate are calculated using the extended Debye-Hueckel method in this example. Values for K_1 , K_2 , and K_{sp} and their variation with temperature were obtained from published values.^(4,5)

Calculating the Simple Index

The calculation of the simple saturation level index requires the following information:

- 1) Analytical values for calcium and total oxalic acid.
- 2) The pH, TDS, and temperature.
- 3) The thermodynamic constants for K_1 and K_2 for oxalic acid
- 4) The K_{sp} for calcium oxalate.
- 5) Activity coefficients for calcium, the oxalate ion.

The thermodynamic constants, activity coefficients, and analytical conversion factors required have been combined in Table 2 and Table 3 to facilitate index calculation. A modification of equation 4 to account for the values included in the tables yields the following simplified formula:

$$\text{Saturation Level} = \frac{\text{Factor 1} [\text{Ca}] [\text{Oxalic acid}_{\text{total}}]}{\text{Factor 2}} \quad (13)$$

where [Ca] is the analytical value for calcium in mg/L as Ca;

[Oxalic acid_{total}] is the analytical value for oxalate in mg/L as C₂O₄;

Factor 1 is the α_2 value from Table 2;

Factor 2 includes the composite thermodynamic properties and conversion factors from Table 3.

The base ten logarithm of the Saturation Level can be used for interpretation, if desired, in the manner in which the Langelier Saturation Index is evaluated.

Adding Calcium oxalate to An Ion Association Model

For increased applicability in varying waters, calcium oxalate Saturation level should be calculated using an ion association model. Ion association models estimate the free ion concentrations prior to index calculation. They account for ‘common ion effects’ and ‘ion pairing.’ It is recommended that the ion pairs for aqueous CaC₂O₄, CaHC₂O₄, MgC₂O₄, and MgHC₂O₄ be added to the calculation matrix and used to adjust the free ion concentrations for calcium and oxalate.

Acknowledgement

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References

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Figure 1: Calcium oxalate pK_{sp} vs Temperature

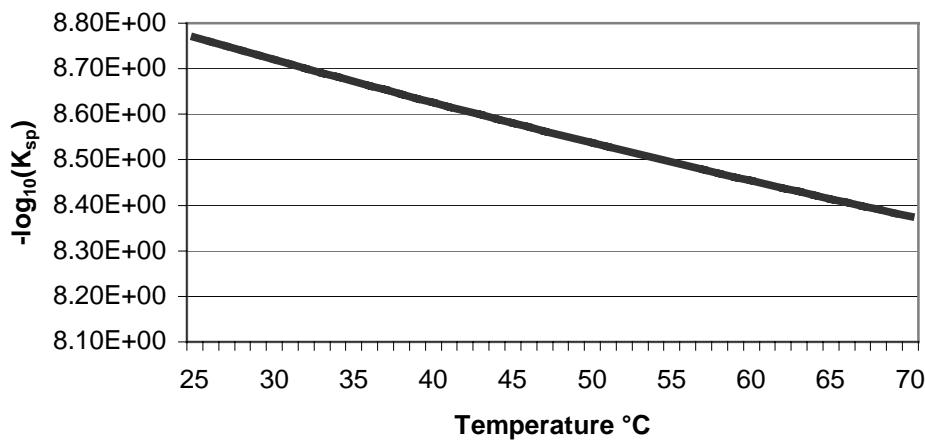


Figure 2: Oxalic acid pK_1 and pK_2 vs Temperature

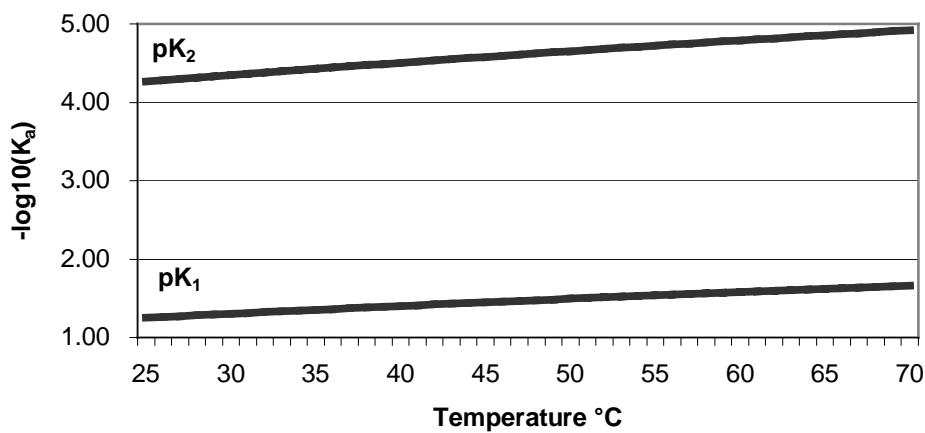


Figure 3: Oxalic acid Distribution vs pH

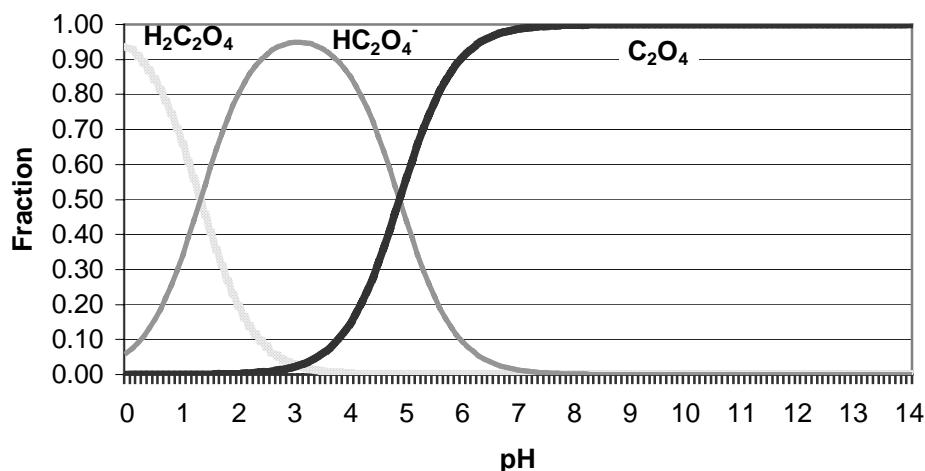


Figure 4: C_2O_4^- Fraction of Total Oxalate vs pH, T

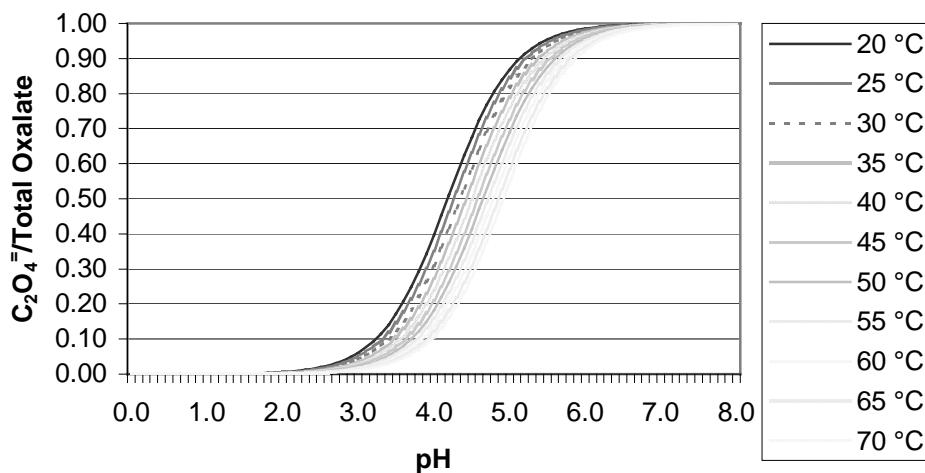


Table 1: Interpreting Indices

| | Saturation Level | $\log_{10}(\text{Saturation Level})$ | Scaling Tendency |
|----------------|------------------|--------------------------------------|----------------------------|
| Supersaturated | > 1.0 | > 0.0 | Scale forms |
| At Equilibrium | 1.0 | 0.0 | Neither forms or dissolves |
| Undersaturated | < 1.0 | < 0.0 | Will tend to dissolve |

Table 2: Oxalate ($C_2O_4^{2-}$) Fraction of Total Oxalic Acid Species versus pH and Temperature

| pH | 20 °C | 25 °C | 30 °C | 35 °C | 40 °C | 45 °C | 50 °C | 55 °C | 60 °C | 65 °C | 70 °C |
|-----|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|
| 1.0 | 0.00026 | 0.00019 | 0.00015 | 0.00011 | 0.00009 | 0.00007 | 0.00005 | 0.00004 | 0.00003 | 0.00003 | 0.00002 |
| 1.2 | 0.00052 | 0.00040 | 0.00031 | 0.00024 | 0.00019 | 0.00015 | 0.00012 | 0.00009 | 0.00008 | 0.00006 | 0.00005 |
| 1.4 | 0.00102 | 0.00080 | 0.00063 | 0.00049 | 0.00039 | 0.00031 | 0.00025 | 0.00020 | 0.00016 | 0.00013 | 0.00011 |
| 1.6 | 0.00188 | 0.00149 | 0.00118 | 0.00095 | 0.00076 | 0.00061 | 0.00050 | 0.00040 | 0.00033 | 0.00027 | 0.00022 |
| 1.8 | 0.00332 | 0.00266 | 0.00214 | 0.00173 | 0.00141 | 0.00115 | 0.00094 | 0.00077 | 0.00064 | 0.00053 | 0.00044 |
| 2.0 | 0.00566 | 0.00458 | 0.00372 | 0.00304 | 0.00249 | 0.00205 | 0.00170 | 0.00141 | 0.00117 | 0.00098 | 0.00082 |
| 2.2 | 0.00941 | 0.00766 | 0.00627 | 0.00515 | 0.00426 | 0.00353 | 0.00295 | 0.00246 | 0.00207 | 0.00175 | 0.00148 |
| 2.4 | 0.01534 | 0.01255 | 0.01032 | 0.00853 | 0.00709 | 0.00592 | 0.00496 | 0.00417 | 0.00353 | 0.00299 | 0.00255 |
| 2.6 | 0.02462 | 0.02023 | 0.01671 | 0.01388 | 0.01158 | 0.00970 | 0.00817 | 0.00691 | 0.00586 | 0.00500 | 0.00428 |
| 2.8 | 0.03899 | 0.03219 | 0.02669 | 0.02224 | 0.01862 | 0.01566 | 0.01323 | 0.01123 | 0.00957 | 0.00818 | 0.00703 |
| 3.0 | 0.06094 | 0.05056 | 0.04212 | 0.03524 | 0.02961 | 0.02498 | 0.02117 | 0.01802 | 0.01540 | 0.01321 | 0.01137 |
| 3.2 | 0.09375 | 0.07829 | 0.06559 | 0.05514 | 0.04653 | 0.03941 | 0.03351 | 0.02860 | 0.02451 | 0.02108 | 0.01820 |
| 3.4 | 0.14130 | 0.11908 | 0.10053 | 0.08507 | 0.07217 | 0.06142 | 0.05244 | 0.04492 | 0.03861 | 0.03331 | 0.02883 |
| 3.5 | 0.17179 | 0.14562 | 0.12353 | 0.10496 | 0.08936 | 0.07627 | 0.06529 | 0.05605 | 0.04827 | 0.04171 | 0.03615 |
| 3.6 | 0.20722 | 0.17683 | 0.15086 | 0.12880 | 0.11012 | 0.09432 | 0.08097 | 0.06970 | 0.06016 | 0.05208 | 0.04522 |
| 3.7 | 0.24775 | 0.21302 | 0.18294 | 0.15707 | 0.13494 | 0.11606 | 0.09999 | 0.08633 | 0.07471 | 0.06482 | 0.05639 |
| 3.8 | 0.29323 | 0.25430 | 0.22003 | 0.19015 | 0.16428 | 0.14199 | 0.12284 | 0.10644 | 0.09240 | 0.08038 | 0.07009 |
| 3.9 | 0.34322 | 0.30048 | 0.26220 | 0.22829 | 0.19851 | 0.17254 | 0.15001 | 0.13053 | 0.11373 | 0.09925 | 0.08679 |
| 4.0 | 0.39692 | 0.35108 | 0.30922 | 0.27147 | 0.23781 | 0.20805 | 0.18191 | 0.15907 | 0.13920 | 0.12194 | 0.10697 |
| 4.1 | 0.45320 | 0.40525 | 0.36052 | 0.31942 | 0.28212 | 0.24863 | 0.21882 | 0.19245 | 0.16925 | 0.14892 | 0.13115 |
| 4.2 | 0.51069 | 0.46180 | 0.41520 | 0.37149 | 0.33108 | 0.29418 | 0.26080 | 0.23088 | 0.20423 | 0.18062 | 0.15978 |
| 4.3 | 0.56789 | 0.51934 | 0.47203 | 0.42671 | 0.38398 | 0.34421 | 0.30765 | 0.27436 | 0.24429 | 0.21732 | 0.19325 |
| 4.4 | 0.62332 | 0.57636 | 0.52958 | 0.48381 | 0.43975 | 0.39795 | 0.35881 | 0.32256 | 0.28933 | 0.25909 | 0.23178 |
| 4.5 | 0.67569 | 0.63140 | 0.58635 | 0.54132 | 0.49707 | 0.45425 | 0.41337 | 0.37485 | 0.33892 | 0.30575 | 0.27535 |
| 4.6 | 0.72400 | 0.68322 | 0.64090 | 0.59774 | 0.55446 | 0.51173 | 0.47014 | 0.43021 | 0.39232 | 0.35674 | 0.32364 |
| 4.7 | 0.76759 | 0.73085 | 0.69203 | 0.65168 | 0.61042 | 0.56889 | 0.52768 | 0.48736 | 0.44840 | 0.41118 | 0.37599 |
| 4.8 | 0.80613 | 0.77370 | 0.73885 | 0.70199 | 0.66362 | 0.62426 | 0.58449 | 0.54484 | 0.50582 | 0.46788 | 0.43140 |
| 4.9 | 0.83962 | 0.81147 | 0.78079 | 0.74784 | 0.71296 | 0.67657 | 0.63913 | 0.60114 | 0.56308 | 0.52542 | 0.48857 |
| 5.0 | 0.86826 | 0.84421 | 0.81767 | 0.78876 | 0.75770 | 0.72479 | 0.69039 | 0.65488 | 0.61870 | 0.58228 | 0.54603 |
| 5.1 | 0.89245 | 0.87216 | 0.84953 | 0.82459 | 0.79745 | 0.76829 | 0.73735 | 0.70493 | 0.67136 | 0.63702 | 0.60228 |
| 5.2 | 0.91264 | 0.89572 | 0.87666 | 0.85545 | 0.83212 | 0.80674 | 0.77947 | 0.75049 | 0.72004 | 0.68843 | 0.65596 |
| 5.4 | 0.94304 | 0.93157 | 0.91847 | 0.90366 | 0.88708 | 0.86871 | 0.84853 | 0.82661 | 0.80302 | 0.77789 | 0.75137 |
| 5.6 | 0.96329 | 0.95571 | 0.94697 | 0.93698 | 0.92566 | 0.91294 | 0.89878 | 0.88313 | 0.86598 | 0.84735 | 0.82729 |
| 5.8 | 0.97652 | 0.97159 | 0.96587 | 0.95929 | 0.95177 | 0.94325 | 0.93366 | 0.92294 | 0.91104 | 0.89794 | 0.88361 |
| 6.0 | 0.98506 | 0.98188 | 0.97819 | 0.97392 | 0.96902 | 0.96343 | 0.95709 | 0.94995 | 0.94197 | 0.93309 | 0.92327 |
| 6.2 | 0.99052 | 0.98849 | 0.98613 | 0.98339 | 0.98023 | 0.97661 | 0.97249 | 0.96783 | 0.96258 | 0.95671 | 0.95018 |
| 6.4 | 0.99400 | 0.99271 | 0.99120 | 0.98945 | 0.98743 | 0.98511 | 0.98246 | 0.97946 | 0.97606 | 0.97224 | 0.96798 |
| 6.6 | 0.99620 | 0.99539 | 0.99443 | 0.99332 | 0.99203 | 0.99055 | 0.98886 | 0.98694 | 0.98476 | 0.98231 | 0.97955 |
| 6.8 | 0.99760 | 0.99708 | 0.99648 | 0.99577 | 0.99496 | 0.99402 | 0.99294 | 0.99172 | 0.99033 | 0.98876 | 0.98700 |
| 7.0 | 0.99849 | 0.99816 | 0.99778 | 0.99733 | 0.99681 | 0.99622 | 0.99554 | 0.99476 | 0.99388 | 0.99288 | 0.99176 |
| 7.2 | 0.99904 | 0.99884 | 0.99860 | 0.99831 | 0.99799 | 0.99761 | 0.99718 | 0.99669 | 0.99613 | 0.99550 | 0.99478 |
| 7.4 | 0.99940 | 0.99927 | 0.99911 | 0.99894 | 0.99873 | 0.99849 | 0.99822 | 0.99791 | 0.99755 | 0.99715 | 0.99670 |
| 8.0 | 0.99985 | 0.99982 | 0.99978 | 0.99973 | 0.99968 | 0.99962 | 0.99955 | 0.99947 | 0.99938 | 0.99928 | 0.99917 |

Use a factor of 1.0 above pH 8.0

Table 3: Composite Factor for Calcium Oxalate Saturation Level versus Temperature, TDS

| °C | TDS 25 | TDS 100 | TDS 250 | TDS 500 | TDS 1000 | TDS 2500 | TDS 5000 |
|-----------|---------------|----------------|----------------|----------------|-----------------|-----------------|-----------------|
| 25 | 7.5077 | 9.2268 | 11.4866 | 14.3588 | 18.9716 | 29.7112 | 43.3730 |
| 26 | 7.6863 | 9.4494 | 11.7679 | 14.7157 | 19.4516 | 30.4837 | 44.5265 |
| 27 | 7.8679 | 9.6760 | 12.0544 | 15.0793 | 19.9409 | 31.2722 | 45.7049 |
| 28 | 8.0526 | 9.9066 | 12.3461 | 15.4497 | 20.4397 | 32.0769 | 46.9087 |
| 29 | 8.2404 | 10.1412 | 12.6430 | 15.8270 | 20.9482 | 32.8980 | 48.1382 |
| 30 | 8.4314 | 10.3798 | 12.9452 | 16.2113 | 21.4665 | 33.7359 | 49.3939 |
| 31 | 8.6256 | 10.6226 | 13.2529 | 16.6026 | 21.9946 | 34.5908 | 50.6762 |
| 32 | 8.8229 | 10.8695 | 13.5659 | 17.0012 | 22.5329 | 35.4629 | 51.9856 |
| 33 | 9.0235 | 11.1206 | 13.8845 | 17.4069 | 23.0813 | 36.3525 | 53.3226 |
| 34 | 9.2274 | 11.3760 | 14.2087 | 17.8201 | 23.6401 | 37.2599 | 54.6876 |
| 35 | 9.4345 | 11.6356 | 14.5385 | 18.2406 | 24.2093 | 38.1854 | 56.0812 |
| 36 | 9.6450 | 11.8995 | 14.8740 | 18.6687 | 24.7891 | 39.1292 | 57.5037 |
| 37 | 9.8588 | 12.1678 | 15.2152 | 19.1044 | 25.3797 | 40.0917 | 58.9557 |
| 38 | 10.0760 | 12.4405 | 15.5622 | 19.5477 | 25.9812 | 41.0730 | 60.4377 |
| 39 | 10.2966 | 12.7177 | 15.9152 | 19.9989 | 26.5937 | 42.0736 | 61.9501 |
| 40 | 10.5207 | 12.9993 | 16.2741 | 20.4580 | 27.2174 | 43.0936 | 63.4936 |
| 41 | 10.7482 | 13.2855 | 16.6390 | 20.9251 | 27.8525 | 44.1335 | 65.0686 |
| 42 | 10.9792 | 13.5762 | 17.0099 | 21.4002 | 28.4990 | 45.1934 | 66.6756 |
| 43 | 11.2137 | 13.8716 | 17.3870 | 21.8835 | 29.1572 | 46.2737 | 68.3152 |
| 44 | 11.4518 | 14.1717 | 17.7704 | 22.3751 | 29.8272 | 47.3748 | 69.9879 |
| 45 | 11.6935 | 14.4764 | 18.1599 | 22.8751 | 30.5091 | 48.4968 | 71.6943 |
| 46 | 11.9387 | 14.7859 | 18.5559 | 23.3835 | 31.2031 | 49.6402 | 73.4350 |
| 47 | 12.1876 | 15.1002 | 18.9582 | 23.9005 | 31.9094 | 50.8053 | 75.2105 |
| 48 | 12.4402 | 15.4193 | 19.3670 | 24.4262 | 32.6281 | 51.9923 | 77.0214 |
| 49 | 12.6965 | 15.7433 | 19.7823 | 24.9606 | 33.3594 | 53.2017 | 78.8683 |
| 50 | 12.9565 | 16.0723 | 20.2043 | 25.5039 | 34.1034 | 54.4337 | 80.7518 |
| 51 | 13.2202 | 16.4062 | 20.6329 | 26.0562 | 34.8603 | 55.6887 | 82.6725 |
| 52 | 13.4877 | 16.7451 | 21.0682 | 26.6175 | 35.6304 | 56.9670 | 84.6311 |
| 53 | 13.7591 | 17.0891 | 21.5104 | 27.1880 | 36.4136 | 58.2691 | 86.6281 |
| 54 | 14.0342 | 17.4382 | 21.9595 | 27.7678 | 37.2103 | 59.5952 | 88.6642 |
| 55 | 14.3133 | 17.7924 | 22.4155 | 28.3570 | 38.0206 | 60.9457 | 90.7400 |
| 56 | 14.5962 | 18.1519 | 22.8785 | 28.9557 | 38.8446 | 62.3209 | 92.8563 |
| 57 | 14.8830 | 18.5165 | 23.3486 | 29.5639 | 39.6826 | 63.7214 | 95.0137 |
| 58 | 15.1738 | 18.8865 | 23.8258 | 30.1819 | 40.5347 | 65.1473 | 97.2129 |
| 59 | 15.4686 | 19.2618 | 24.3103 | 30.8097 | 41.4011 | 66.5992 | 99.4546 |
| 60 | 15.7674 | 19.6424 | 24.8021 | 31.4475 | 42.2820 | 68.0773 | 101.7394 |
| 61 | 16.0702 | 20.0285 | 25.3013 | 32.0953 | 43.1775 | 69.5821 | 104.0682 |
| 62 | 16.3771 | 20.4201 | 25.8079 | 32.7532 | 44.0879 | 71.1141 | 106.4416 |
| 63 | 16.6880 | 20.8171 | 26.3221 | 33.4214 | 45.0134 | 72.6735 | 108.8604 |
| 64 | 17.0031 | 21.2197 | 26.8438 | 34.1000 | 45.9540 | 74.2608 | 111.3253 |
| 65 | 17.3223 | 21.6279 | 27.3732 | 34.7891 | 46.9101 | 75.8765 | 113.8372 |
| 66 | 17.6457 | 22.0418 | 27.9103 | 35.4888 | 47.8819 | 77.5209 | 116.3969 |
| 67 | 17.9733 | 22.4614 | 28.4553 | 36.1992 | 48.8694 | 79.1945 | 119.0050 |
| 68 | 18.3051 | 22.8867 | 29.0082 | 36.9205 | 49.8730 | 80.8977 | 121.6625 |
| 69 | 18.6412 | 23.3178 | 29.5690 | 37.6527 | 50.8928 | 82.6309 | 124.3702 |
| 70 | 18.9816 | 23.7547 | 30.1379 | 38.3961 | 51.9291 | 84.3948 | 127.1289 |

